

CHAPTER 22 PROBLEM SOLUTIONS

SOLUTION TO PROBLEM 22.1

(a) For figure P22.1a, $T_0 = 2$ and $\phi_0 = \pi$. Let $t_0 = -1$ in equation 22.5b. Then $f(t) = 0.5 - (t - 1)$ and

$$c_n = 0.5 \int_{-1}^1 \delta(t) e^{-jn\pi t} dt = 0.5 \int_{-1}^1 e^{-jn\pi t} dt = 0.5 \left[\frac{e^{-jn\pi t}}{-jn\pi} \right]_{-1}^1 = 0.5 \frac{e^{-jn\pi} - e^{jn\pi}}{-jn\pi} = 0.5 \frac{2j \sin(n\pi)}{-jn\pi} = 0.5 \frac{2 \sin(n\pi)}{n\pi}$$

From equation 22.6, $a_n = 1$ and $b_n = 0$ for all n . Finally from equation 22.2

$$f(t) = 0.5 + \sum_{n=1}^{\infty} \frac{1}{n\pi} \cos(n\pi t)$$

(b) For figure P22.1b, $T_0 = 2$ and $\phi_0 = \pi$. Let $t_0 = 0$ in equation 22.5b. Then $f(t) = -0.5(t - 1)$ and

$$c_n = -0.5 \int_{-1}^1 \delta(t - 1) e^{-jn\pi t} dt = -0.5 e^{-jn\pi} = -0.5 (-1)^n$$

From equation 22.6, $b_n = 0$ for all n , and

$$a_n = -1 \text{ for } n \text{ even}$$

$$a_n = 1 \text{ for } n \text{ odd}$$

Finally from equation 22.2

$$f(t) = -0.5 + \cos(\pi t) - \cos(2\pi t) + \cos(3\pi t) - \cos(4\pi t) + \dots$$

SOLUTION TO PROBLEM 22.2

(a) $T_0 = 1$ and $\phi_0 = 2\pi$. Let $t_0 = 0$ in equation 22.5b. Then

$$f(t) = e^{-(\ln 2)t}$$

and from equation 22.5b

$$c_n = \int_0^1 e^{-(\ln 2)t} e^{-j2n\pi t} dt = \int_0^1 e^{-(\ln 2 + j2n\pi)t} dt = \frac{-1}{(\ln 2 + j2n\pi)} \left[e^{-(\ln 2 + j2n\pi)t} - 1 \right]$$

$$= \frac{0.5}{(\ln 2 + j2n\pi)}$$

(b) Using the above result for c_n

$$c_0 = \frac{0.5}{\ln 2} = 0.7213,$$

$$c_1 = \frac{0.5}{\ln 2 + j2\pi} = 0.7213 e^{-j1.4609}$$

$$c_2 = \frac{0.5}{\ln 2 + j4\pi} = 0.397 e^{-j1.516}$$

From equation 22.6

$$d_0 = c_0 = 0.7213$$

$$d_1 = 2|c_1| = 0.158,$$

$$\phi_1 = -1.461 \times 180^\circ = -83.7^\circ$$

$$d_2 = 2|c_2| = 0.0795$$

$$\phi_2 = -1.516 \times 180^\circ = -86.84^\circ$$

Thus, $f(t)$ in the form of equation 22.3 is

$$f(t) = 0.7213 + 0.158\cos(2\pi t - 83.7^\circ) + 0.0795\cos(2\pi t - 86.84^\circ)$$

SOLUTION TO PROBLEM 22.3.

(a) $T_0 = 1$ and $\omega_0 = 2$. Let $t_0 = 0$ in equation 22.5b. Then

$$f(t) = e^{-(\ln(2))t} [u(t) - u(t - 0.5)]$$

and from equation 22.5b

$$c_n = \int_0^{0.5} e^{-(\ln(2))t} e^{-j2n\pi t} dt = \int_0^{0.5} e^{-(\ln(2) + j2n\pi)t} dt = \frac{-1}{(\ln(2) + j2n\pi)} \left[e^{-0.5(\ln(2) + j2n\pi)} - 1 \right]$$

$$= \frac{1 - \frac{(-1)^n}{\sqrt{2}}}{(\ln(2) + j2n\pi)}$$

(b) Using the above result for c_n , and MATLAB to evaluate the numerical result,

```

>>n=0;
>>c0=(1-(-1)^n/sqrt(2))/(log(2)+j*2*n*pi)
c0
 4.2256e-01
>>n=1;
>>c1=(1-(-1)^n/sqrt(2))/(log(2)+j*2*n*pi)
c1 =
 2.9612e-02- 2.6843e-01i
>>abs(c1)
ans =
 2.7006e-01
>>degreec1=angle(c1)*180/pi
degreec1 =
-8.3705e+01
>>n=2;
>>c2=(1-(-1)^n/sqrt(2))/(log(2)+j*2*n*pi)
c2 =
 1.2817e-03- 2.3237e-02i

```

```

»abs(c2)
ans =
    2.3272e-02
degreec2= angle(c2)*180/pi
degreec2 =
   -8.6843e+01

```

From equation 22.6 and equation 22.3

$$f(t) = 0.4226 + 0.54\cos(2t - 83.7^\circ) + 0.04654\cos(2t - 86.84^\circ)$$

SOLUTION PROBLEM 22.4. (a) $f(t) = \cos(4t) \sin(2t) = 0.5[\sin(6t) - \sin(2t)]$.

The fundamental angular frequency of $f(t)$ is $\omega_0 = 2$ rad/s. The given $f(t)$ can be expressed as $f(t) = -0.5 \sin(\omega_0 t) + 0.5 \sin(3\omega_0 t)$. Observe that $b_1 = -0.5$, $b_3 = 0.5$ and all other a_j and b_j are zero.

From equation 22.4, $d_1 = 0.5 \angle -90^\circ$ and $d_3 = 0.5 \angle 90^\circ$. From equations 22.6a and 22.6b.

$c_1 = 0.25j$ and $c_3 = -0.25j$. All other c_n are zero for n positive

$$\begin{aligned} \text{(b) } f(t) &= \sin^2(4t) \cos^2(8t) = 0.5[1 - \cos(8t)] \times 0.5[1 + \cos(16t)] \\ &= 0.25 [1 - \cos(8t) + \cos(16t) - \cos(8t) \cos(16t)] \\ &= 0.25 - 0.375 \cos(8t) + 0.25 \cos(16t) - 0.125 \cos(24t) \end{aligned}$$

The fundamental angular frequency of $f(t)$ is $\omega_0 = 8$ rad/s. The given $f(t)$ can be expressed as

$f(t) = 0.25 - 0.375 \cos(\omega_0 t) + 0.25 \cos(2\omega_0 t) - 0.125 \cos(3\omega_0 t)$. Observe that $a_0 = 0.25$, $a_1 = -0.375$, $a_2 = 0.25$, $a_3 = -0.125$ and all other a_j and b_j are zero.

From equation 22.4,

$$d_0 = 0.25, d_1 = 0.375 \angle 180^\circ, d_2 = 0.25 \angle 0^\circ, \text{ and } d_3 = 0.125 \angle 180^\circ,$$

From equations 22.6a and 22.6b.

$$c_0 = 0.25, c_1 = -0.375 \text{ and } c_2 = 0.25, c_3 = -0.125. \text{ All other } c_n \text{ are zero for } n \text{ positive.}$$

(c)

$$\begin{aligned} f(t) &= [2 + 1.5 \sin(500t) - 2 \cos(2000t)] \cos(10^6 t) \\ &= 2 \cos(10^6 t) + 0.75 \sin(1000500t) + 0.75 \sin(999500t) \\ &\quad - \cos(1002000t) - \cos(998000t) \end{aligned}$$

The fundamental angular frequency of $f(t)$ is $\omega_0 = 500$ rad/s. The given $f(t)$ can be expressed as

$$f(t) = 2 \cos(2000 \omega_0 t) + 0.75 \sin(2001 \omega_0 t) + 0.75 \sin(1999 \omega_0 t) - \cos(2004 \omega_0 t) - \cos(1996 \omega_0 t)$$

Observe that: $a_{1996} = -1$, $b_{1999} = 0.75$, $a_{2000} = 2$, $b_{2001} = 0.75$, $a_{2004} = -1$, and all other a_j and b_j are zero.

From equation 22.4, $d_{1996} = 1 \angle 180^\circ$, $d_{1999} = 0.75 \angle -90^\circ$, $d_{2000} = 2 \angle 0^\circ$,

$d_{2001} = 0.75 \angle -90^\circ$, $d_{2004} = 1 \angle 180^\circ$, and all other d_j are zero.

From equations 22.6a and 22.6b.

$$c_{1996} = -0.5, c_{1999} = -j0.375, c_{2000} = 1,$$

$c_{2001} = -j0.375^0$, $dc_{2004} = -0.5$, and all other c_n are zero for n positive..

SOLUTION PROBLEM 22.5

By inspection, the derivative of $f(t)$ is

$$f'(t) = \frac{A}{T} - \sum_{n=-\infty}^{\infty} A \delta(t - nT) = \frac{A}{T} - f_{\delta}(t)$$

where $f(t)$ is shown in figure 22/7, with its Fourier series given by equation 22.20b, i.e.

$$f_{\delta}(t) = \frac{A}{T} + \sum_{n=1}^{\infty} \frac{2A}{T} \cos(n\omega_0 t)$$

Therefore

$$f'(t) = -\sum_{n=1}^{\infty} \frac{2A}{T} \cos(n\omega_0 t)$$

The dc component is the average value of $f(t)$ and is given by $0.5A$. Other terms in the Fourier series of $f(t)$ are obtained by integrating the cosine terms in the above expression. The result is

$$f(t) = 0.5A - \sum_{n=1}^{\infty} \frac{A}{n} \sin(n\omega_0 t)$$

SOLUTION TO PROBLEM 22.6

Denote by $f_5(t)$ the waveform of figure P22.5, with $A=0.5$ and $T=1$. Then by inspection

$$f(t) = f_{prob5}(-t) + 0.5$$

Substituting the result of problem 22.5 into the above equation, we have

$$f(t) = 0.75 + \sum_{n=1}^{\infty} \frac{0.5}{n} \sin(n\omega_0 t)$$

SOLUTION PROBLEM 22.7

Consider the square wave $g(t)$ shown in figure 22.4 with its Fourier series given by equation 22.13. By inspection, the derivative of $f(t)$ is

$$f'(t) = -\frac{4}{T} g(t) \quad f(t) = -\frac{4}{T} g(t)$$

Substituting equation 22.13 into the above expression, we have

$$f'(t) = -\frac{8A}{T} \sum_{n=1, \text{ odd}} \frac{\sin(n\omega_0 t)}{n}$$

The dc component is the average value of $f(t)$ and is given by $0.5A$. Other terms in the Fourier series of $f(t)$ are obtained by integrating the sine terms in the above expression. The result is

$$f(t) = 0.5A + \frac{4A}{2} \sum_{n=1, \text{ odd}} \frac{\cos(n\omega_0 t)}{n^2}$$

SOLUTION PROBLEM 22.8

The method used below is simpler than that suggested in the hint.

We first sketch the waveform of $f'(t)$ and observe that it may be expressed as the sum of two periodic rectangular pulse trains:

$$f'(t) = \frac{1}{T} [f_p(t + 0.5T) + f_p(t - 0.5T)]$$

where $f_p(t)$ is sketched in figure 22.8. Using equation 22.23, we have

$$\begin{aligned} f'(t) &= \frac{1}{T} \left\{ \left[A + \sum_{n=1} \frac{2A \sin(n\omega_0 T/2)}{n} \cos(n\omega_0(t + 0.5T)) \right] \right. \\ &\quad \left. - \left[A + \sum_{n=1} \frac{2A \sin(n\omega_0 T/2)}{n} \cos(n\omega_0(t - 0.5T)) \right] \right\} \\ &= \frac{1}{T} \sum_{n=1} \frac{2A \sin(n\omega_0 T/2)}{n} [\cos(n\omega_0(t + 0.5T)) - \cos(n\omega_0(t - 0.5T))] \end{aligned}$$

$$= \frac{1}{T} \left[\sum_{n=1}^{\infty} \frac{-4A \sin^2(n \omega_0 t)}{n} \sin(n \omega_0 t) \right]$$

The dc component is the average value of $f(t)$ and is given by A . Other terms in the Fourier series of $f(t)$ are obtained by integrating the sine terms in the above expression. The result is

$$f(t) = A + \frac{2A}{2} \sum_{n=1}^{\infty} \left[\frac{\sin(n \omega_0 t)}{n} \right]^2 \cos(n \omega_0 t)$$

SOLUTION TO PROBLEM 22.9

We first sketch the waveform of $f(t)$ and observe that it may be expressed as the sum of a periodic rectangular pulse train and a periodic impulse train:

$$f(t) = \frac{1}{T} f_p(t + 0.5 T) - f(t)$$

where $f_p(t)$ is sketched in figure 22.8, and $f(t)$ in figure 22.7.

Using equations 22.23 and 22.20b, we have

$$f(t) = \frac{1}{T} \left[A + \sum_{n=1}^{\infty} \frac{2A \sin(n \omega_0 t)}{n} \cos(n \omega_0 (t + 0.5 T)) \right] - \left[\frac{A}{T} + \sum_{n=1}^{\infty} \frac{2A}{T} \cos(n \omega_0 t) \right]$$

$$= \frac{2A}{T} \left\{ \sum_{n=1}^{\infty} \left[\frac{\sin(n \omega_0 t)}{n} \cos(n \omega_0 (t + 0.5 T)) - \cos(n \omega_0 t) \right] \right\}$$

The dc component is the average value of $f(t)$ and is given by $0.5 A$. Other terms in the Fourier series of $f(t)$ are obtained by integrating the sine terms in the above expression. The result is

$$f(t) = 0.5 A + \frac{A}{n} \sum_{n=1}^{\infty} \left[\frac{\sin(n \omega_0 t)}{n} \sin(n \omega_0 (t + 0.5 T)) - \sin(n \omega_0 t) \right]$$

It remains to rewrite the expression in the form of equation 22.2.

To this end, let $b = \sin(n \omega_0 t) / (n \omega_0)$ and re-write the terms within [] as follows:

$$b \sin(n \omega t) \cos(n \omega t) + \{b \cos(n \omega t) - 1\} \sin(n \omega t)$$

Hence, $f(t)$ in the form of equation 22.2 has the coefficients, for $n=1,2,\dots$

$$a_n = -\frac{A}{2n^2} \sin^2(n \omega t)$$

$$b_n = -\frac{A}{2n^2} \{ \sin(n \omega t) \cos(n \omega t) - n \omega t \}$$

$$d_n = \sqrt{a_n^2 + b_n^2} = -\frac{A}{2n^2} \sqrt{\sin^4(n \omega t) + \{ \sin(n \omega t) \cos(n \omega t) - n \omega t \}^2}$$

$$= -\frac{A}{2n^2} \sqrt{\sin^2(n \omega t) + (n \omega t)[n \omega t - \sin(2n \omega t)]}$$

$$\phi_n = \tan^{-1}\left(\frac{-b_n}{a_n}\right)$$

The result is item 6 of table 22.4

SOLUTION PROBLEM 22.10.

Observe that the present $f(t)$ can be derived from that of problem 22.9 by (a) replacing t by $-t$; and (b) replacing ω by ω . Thus the Fourier series for $f(t)$ is:

$$f(t) = 0.5 A + \sum_{n=1}^{\infty} [a_n \cos(n \omega t) + b_n \sin(n \omega t)]$$

where

$$a_n = -\frac{A}{2n^2} \sin^2(n \omega t)$$

$$b_n = -\frac{-A}{2n^2} \{ \sin(n \omega t) \cos(n \omega t) - n \omega t \}$$

$$d_n = \sqrt{a_n^2 + b_n^2} = -\frac{A}{2n^2} \sqrt{\sin^4(n \omega t) + \{ \sin(n \omega t) \cos(n \omega t) - n \omega t \}^2}$$

$$= -\frac{A}{2n^2} \sqrt{\sin^2(n \omega t) + (n \omega t)[n \omega t - \sin(2n \omega t)]}$$

$$\phi_n = \tan^{-1}\left(\frac{-b_n}{a_n}\right)$$

SOLUTION PROBLEM 22.11. Following the hint, we have the second derivative of $f(t)$ given by

$$f''(t) = \frac{1}{\alpha(1-\alpha)T} f_{\delta}(t + \alpha T) - \frac{1}{\alpha(1-\alpha)T} f_{\delta}(t)$$

where $f_{\delta}(t)$ is given in example 22.5. Notice that we have focused on the part of the waveform over $[-T, (1-\alpha)T]$. By making use of equation 22.20b, we obtain

$$\begin{aligned} f''(t) &= \frac{2A}{\alpha(1-\alpha)T^2} \sum_{n=1}^{\infty} [\cos(n\omega_0 t + 2n\alpha) - \cos(n\omega_0 t)] \\ &= \frac{-4A}{\alpha(1-\alpha)T^2} \sum_{n=1}^{\infty} [\sin(n\omega_0 t + n\alpha) \sin(n\alpha)] \end{aligned}$$

Therefore,

$$\begin{aligned} f(t) &= [f(t)]_{ave} + \frac{4A}{\alpha(1-\alpha)T^2} \sum_{n=1}^{\infty} \frac{\sin(n\alpha)}{(n\omega_0)^2} \sin(n\omega_0 t + n\alpha) \\ &= \frac{A}{2} + \sum_{n=1}^{\infty} \frac{A \sin(n\alpha)}{n^2 \alpha(1-\alpha)} \cos(n\omega_0 t + (n\alpha - 0.5)) \end{aligned}$$

Letting $T = 1$ and $\alpha = 0.25$ we obtain,

$$f(t) = \frac{A}{2} + \sum_{n=1}^{\infty} \frac{16A \sin \frac{n\pi}{4}}{3n^2} \cos(n2\pi t + (0.25n - 0.5)\pi)$$

Therefore, $d_0 = 0.5A$, and

$$d_n = \frac{16A \sin \frac{n\pi}{4}}{3n^2}$$

It follows that $d_1 = 0.38211A$ and $d_2 = 0.13509A$.

SOLUTION TO PROBLEM 22.12.

Denote by $f_p(t)$ the period rectangular waveform of figure 22.5, with $A=1$.

Then we can express the present $f(t)$, with $T= 4$, as the sum of 3 terms:

$$f(t) = 3f_p(t-0.125T, 0.25) + 4 f_p(t - 0.5T, 0.5) - 2$$

From equation 22.14b, and equation 22.12c, for $n= 1,2,\dots$

$$\begin{aligned} c_n &= \frac{3}{n} \sin(0.25n) e^{-jn} \times 0.125T + \frac{4}{n} \sin(0.5n) e^{-jn} \times 0.5T \\ &= \frac{3}{n} \sin(0.25n) e^{-j0.25n} + \frac{4}{n} \sin(0.5n) e^{-jn} \end{aligned}$$

The numerical values of the first few Fourier series coefficients are:

$$\begin{aligned} c_0 &= \text{average value of } f(t) = \frac{1}{4}(1 + 4 - 2) = 0.75 \\ c_1 &= \frac{3}{1} \sin(0.25) e^{-j0.25} + \frac{4}{1} \sin(0.5) e^{-j} = -0.7958 - j 0.4775 \\ c_2 &= \frac{3}{2} \sin(0.5) e^{-j0.5} + \frac{4}{2} \sin(1) e^{-j2} = -j0.4775 \end{aligned}$$

Solution Problem 22.13

(a) For sinusoidal steady analysis, the transfer function is

$$H(j\omega) = \frac{Y_L}{Y_L + Y_C + Y_R} = \frac{1}{1 + Z_L Y_C + Z_L Y_R} = \frac{1}{(1 - \omega^2 LC) + j \frac{L}{R} \omega} = \frac{1}{(1 - 4 \times 10^{-5} \omega^2) + j \times 10^{-3} \omega}$$

The transfer function evaluated at various input frequencies are listed below.

$$H(0) = 1$$

$$H(j377) = 0.2128 \angle -175.4^\circ$$

$$H(j3 \times 377) = 0.0199 \angle -178.7^\circ$$

$$H(j5 \times 377) = 0.0071 \angle -179.2^\circ$$

Using equation 15.7 and superposition, we obtain the steady state output voltage (in V):

$$\begin{aligned} v_{\text{out}}(t) &= 200 + 200\sqrt{2} \times 0.2128 \cos(377t - 175.4^\circ) + 60\sqrt{2} \times 0.0199 \cos(3 \times 377t + 30^\circ - 178.7^\circ) \\ &\quad + 80\sqrt{2} \times 0.0071 \cos(5 \times 377t + 50^\circ - 179.2^\circ) \end{aligned}$$

$$= 200 + \sqrt{2} \times 42.55 \cos(377t - 175.4^\circ) + \sqrt{2} \times 1.196 \cos(3 \times 377t - 148.7^\circ) \\ + \sqrt{2} \times 0.5668 \cos(5 \times 377t - 129.2^\circ)$$

(b) From equation derived in P11.39,

$$V_{\text{out,eff}} = \sqrt{200^2 + 42.55^2 + 1.196^2 + 0.5668^2} = 204.48 \text{ V}$$

The average power absorbed by the 10 k resistor is

$$P_{\text{av}} = \frac{204.48^2}{10^4} = 4.1812 \text{ W}$$

Solution Problem 22.14

One correction in the problem statement: in the angle expression, 5000 should be 10000.

(a) Using the identity $\cos(x)\cos(y) = 0.5\cos(x+y) + 0.5\cos(x-y)$, we have

$$v_{\text{in}}(t) = 0.1\cos(998,000t) + 0.2\cos(999,000t) + 2\cos(1,000,000t) \\ + 0.2\cos(1,001,000t) + 0.1\cos(1,002,000t) \quad \text{V}$$

(b) The transfer function has a constant magnitude of 10, and a phase shift proportional to the deviation from ω_c . at $\omega = \omega_c + 2 \text{ m}$, the phase shift is -9 degrees. From these facts, we can write directly

$$v_{\text{out}}(t) = \cos(998,000t + 9^\circ) + 2\cos(999,000t + 4.5^\circ) + 20\cos(1,000,000t) \\ + 2\cos(1,001,000t - 4.5^\circ) + \cos(1,002,000t - 9^\circ) \quad \text{V}$$

(c) Using the identity

$$\cos(x)\cos(y) = 2 \cos\left(\frac{x+y}{2}\right)\cos\left(\frac{x-y}{2}\right)$$

we can group the terms in $v_{out}(t)$ and re-write it as

$$\begin{aligned} v_{out}(t) &= 2 \cos(2 \text{ m}t - 9^\circ)\cos(\text{ c}t) + 4\cos(\text{ m}t - 4.5^\circ)\cos(\text{ c}t) + 20\cos(\text{ c}t) \\ &= [20 + 4\cos(\text{ m}t - 4.5^\circ) + 2 \cos(2 \text{ m}t - 9^\circ)]\cos(\text{ c}t) = g(t)\cos(\text{ c}t) \end{aligned}$$

Thus

$$g(t) = 20 + 4\cos(\text{ m}t - 4.5^\circ) + 2\cos(2 \text{ m}t - 9^\circ)$$

With $t_d = 78.54 \mu\text{s}$, then $\text{ m}t_d = 1000 \times 78.54 \times 10^{-6} = 0.07854 \text{ rad}$, or 4.5 degrees. We have

$$\begin{aligned} 10 f(t - t_d) &= 20[1 + 0.2\cos(\text{ m}(t - t_d)) + 0.1\cos(2 \text{ m}(t - t_d))] \\ &= 20[1 + 0.2\cos(\text{ m}t - 4.5^\circ) + 0.1 \cos(2 \text{ m}t - 9^\circ)] = g(t) \end{aligned}$$

SOLUTION PROBLEM 22.15. (a) This proof is a special case of the general proof given in the solution to Problem 22.16. See the solution to problem 22.16, below.

FOR THE REMAINING PARTS, WE USE THE FOLLOWING MATLAB CODE:

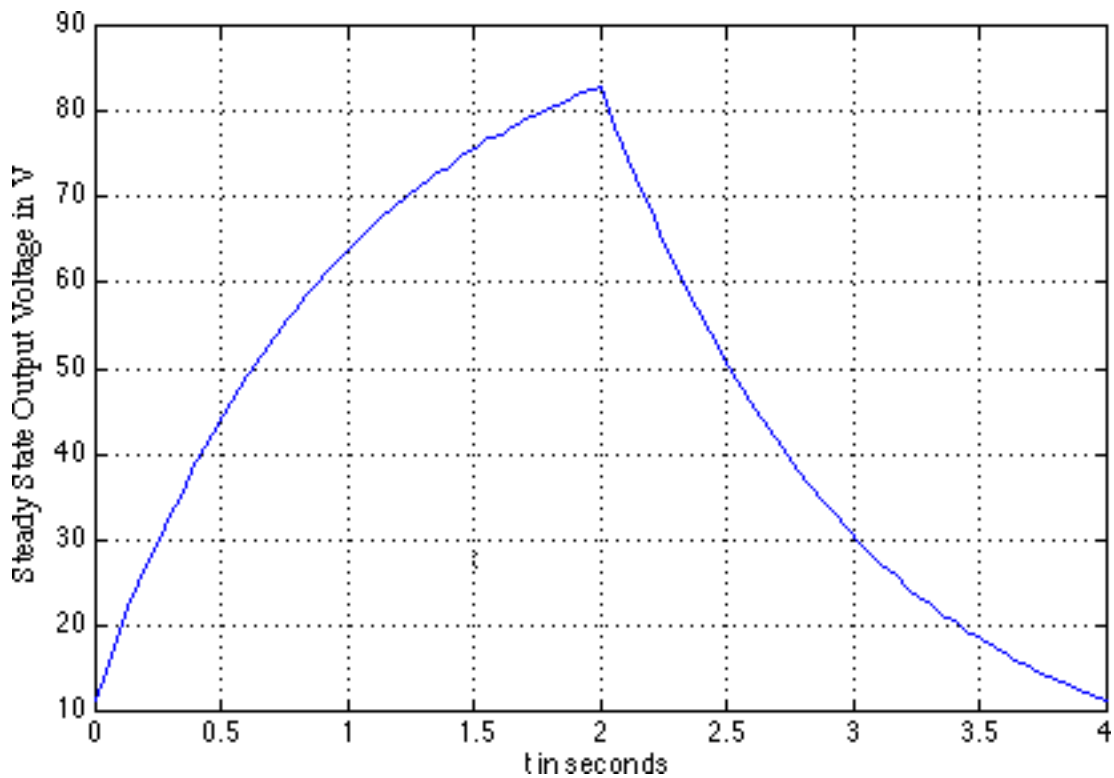
```
% chapter 22, problem 15.
%part (b).
Vmax= 30*pi;
Vmin=0;
T=4;R = 1; C = 1;
voutmin= Vmin+(Vmax - Vmin)/(1+ exp(0.5*T/(R*C)))
voutmax = Vmax - (Vmax -Vmin)/(1+ exp(0.5*T/(R*C)))
t1= 0: 0.05: 2;
vseg1= Vmax+(voutmin- Vmax)*exp((-t1/(R*C)));
t2= 2:0.05: 4;
vseg2= Vmin+(voutmax- Vmin)*exp(-(t2-T/2)/(R*C));
t= [ t1 t2];
v= [vseg1 vseg2];
plot(t,v)
grid
xlabel('t in seconds')
ylabel('Steady State Output Voltage in V')
```

%part (c)
 error1= 100*(12.235- voutmin)/voutmin
 error2= 100*(82.013 - voutmax)/voutmax

TO OBTAIN

(b)
 voutmin =
 1.1235e+01
 voutmax =
 8.3013e+01

(c)
 error1 =
 8.9045e+00
 error2 =
 -1.2048e+00



SOLUTION PROBLEM 22.16. CORRECTION: In the problem statement, $\frac{s}{\tau}$ should be τs .

For simplicity, let us consider the case when the transfer function is a voltage ratio, i.e., $H(s) = V_{out}/V_{in}$.

If a constant input $v_{in}(t) = V_{con}$ is applied to the stable network, then the $v_{out}() = KV_{con}$,

independent of the initial conditions. This is because the zero-input response for a stable network approaches zero as t approaches infinite. To see this observe that the zero-state response is given by

$$v_{out}(t) = L^{-1} \frac{K/\tau}{s + 1/\tau} \times \frac{V_{con}}{s} = L^{-1} \frac{KV_{con}}{s} - \frac{KV_{con}}{s + 1/\tau} = KV_{con} \left(1 - e^{-t/\tau}\right) u(t)$$

from which $v_{out}(\infty) = KV_{con}$ as asserted.

For the remainder of our proof we make use of the fact that in steady state, $v_{out}(t+T) = v_{out}(t)$ with $t = 0$ in our case. Specifically, after the first order network has reached steady state, the $v_{out}(t)$ waveform will be periodic as shown in figure P22.15c, where the time reference has been chosen so that $v_{out,min}$ occurs at $t = 0$.

Recall equation 8.19

$$x(t) = x(t_0^-) + \left[x(t_0^+) - x(t_0^-) \right] e^{-(t-t_0)/\tau}$$

Applying this equation to the interval $[0, T/2]$, we have

$$b_0 = KV_{max} + (a_0 - KV_{max}) e^{-0.5T/\tau} = KV_{max} + (a_0 - KV_{max}) \alpha \quad (1)$$

Note that $\alpha = e^{-0.5T/\tau}$. Similarly, applying equation 8.19 to the interval $[T/2, T]$ leads to

$$a_0 = KV_{min} + (b_0 - KV_{min}) \alpha \quad (2)$$

Equations (1) and (2) can be written as a single matrix equation

$$\begin{bmatrix} -\alpha & 1 \\ 1 & -\alpha \end{bmatrix} \begin{bmatrix} a_0 \\ b_0 \end{bmatrix} = \begin{bmatrix} (1-\alpha)KV_{max} \\ (1-\alpha)KV_{min} \end{bmatrix} \quad (3)$$

Solving equation (3) by matrix inverse (or Cramer's rule) results in

$$\begin{bmatrix} a_0 \\ b_0 \end{bmatrix} = \frac{-1}{\alpha^2 - 1} \begin{bmatrix} \alpha & 1 \\ 1 & \alpha \end{bmatrix} \begin{bmatrix} (1-\alpha)KV_{max} \\ (1-\alpha)KV_{min} \end{bmatrix} = \frac{K}{\alpha + 1} \begin{bmatrix} \alpha & 1 \\ 1 & \alpha \end{bmatrix} \begin{bmatrix} V_{max} \\ V_{min} \end{bmatrix} = \frac{K}{\alpha + 1} \begin{bmatrix} \alpha V_{max} + V_{min} \\ V_{max} + \alpha V_{min} \end{bmatrix}$$

$$[v_{out}(t)]_{min} = a_0 = K \frac{\alpha V_{max} + V_{min}}{\alpha + 1} = K \frac{\alpha V_{max} + V_{min} + \alpha V_{min} - \alpha V_{min}}{\alpha + 1}$$

$$= KV_{min} + \alpha \frac{V_{max} - V_{min}}{\alpha + 1} = KV_{min} + K \frac{V_{max} - V_{min}}{1 + 1/\alpha} = KV_{min} + K \frac{V_{max} - V_{min}}{1 + e^{0.5T/\tau}}$$

and

$$\begin{aligned}
 [v_{out}(t)]_{\max} = b_0 &= K \frac{V_{\max} + \alpha V_{\min}}{\alpha + 1} = K \frac{V_{\max} + \alpha V_{\min} + \alpha V_{\max} - \alpha V_{\max}}{\alpha + 1} \\
 &= KV_{\max} - K \frac{V_{\max} - V_{\min}}{1 + 1/\alpha} = KV_{\max} - K \frac{V_{\max} - V_{\min}}{1 + e^{0.5T/\tau}}
 \end{aligned}$$

This complete completes the derivation of the desired formulas.

SOLUTION TO PROBLEM 22.17

There is one correction in the problem statement. 1-kHz should be 5.1mHz.

(a) The transfer function is, according to equation 4.3, and using the given element values $R_1 = 10 \text{ k}$,
 $R_f = 50 \text{ k}$ and $C = 20 \text{ mF}$:

$$H(s) = \frac{V_{out}}{V_{in}} = -\frac{Z_f}{Z_1} = -\frac{Y_1}{Y_f} = -\frac{\frac{1}{R_1}}{C_s + \frac{1}{R_f}} = -\frac{\frac{R_f}{R_1}}{1 + R_f C_s} = \frac{-5}{1 + 1000s}$$

(b) Here we have We have $K = -5$, $t = 1000 \text{ s}$, $V_{\max} = 1 \text{ V}$, $V_{\min} = -1 \text{ V}$ and $T = 1/f = 1/0.0051 = 196.15 \text{ s}$. In using the equations derived in problem 22.16, we note that the subscripts min and max should be switched in this case because K is negative. The following MATLAB codes perform the needed numerical calculations.

```

f= 5.1e-3;
Cf=20e-3;
Rf=50e3;
Rs= 10e3;
T=1/f;
K= -Rf/Rs;
tau=Rf*Cf;
['part (b)']
Vmax=1;
Vmin=-1;
voutmax= K*( Vmin + (Vmax-Vmin)/(1+exp(0.5*T/tau)))
voutmin= K*( Vmax - (Vmax-Vmin)/(1+exp(0.5*T/tau)))

```

answers from MATLAB are:

```

voutmax =
    0.2449
voutmin =
   -0.2449

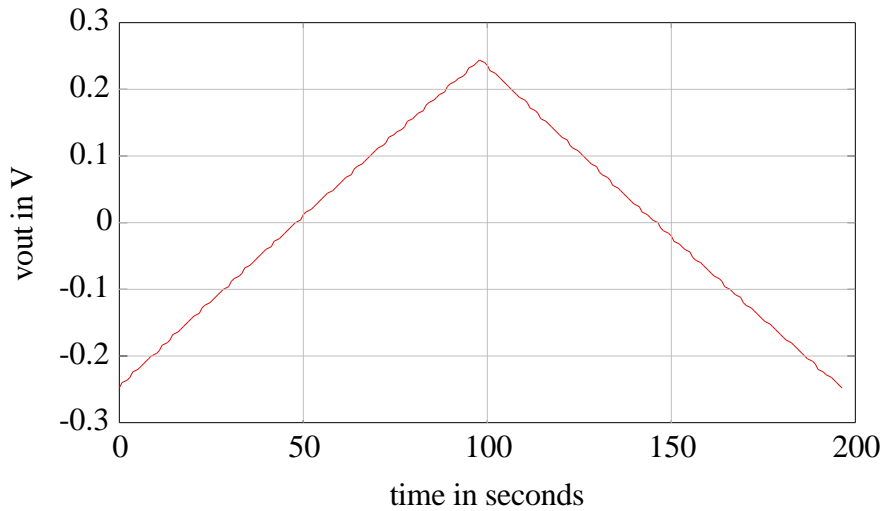
```

(c)
['part (c)']

```

t1= 0:0.005*T:0.5*T;
v1= 5 + (-0.245 -5).*exp(-(t1/tau)) ;
t2= 0.5*T:0.005*T:T;
v2= -5 + (0.245 +5).*exp(-(t2-0.5*T)/tau) ;
t=[t1,t2];
v=[v1,v2];
plot (t,v)
xlabel('time in seconds')
ylabel('vout in V')
grid

```



SOLUTION PROBLEM 22.18.

$$v_i(t) = \cos(\omega t) = \cos(6000t)$$

$$\begin{aligned}
v_o(t) &= 10v_i + v_i^2 + v_i^3 \\
&= 10\cos(\omega t) + \cos^2(\omega t) + \cos^3(\omega t) \\
&= 10\cos(\omega t) + 0.5 + 0.5\cos(2\omega t) + 0.75\cos(\omega t) + 0.25\cos(3\omega t) \\
&= 0.5 + 10.75 \cos(\omega t) + 0.5\cos(2\omega t) + 0.25\cos(3\omega t)
\end{aligned}$$

The effective values of various components of the output are:

dc	fundamental	2nd harmonic	3rd harmonic	total harmonic
0.5	10.75/ $\sqrt{2}$	0.5/ $\sqrt{2}$	0.25/ $\sqrt{2}$	0.559/ $\sqrt{2}$

The total harmonic distortion is

$$\frac{0.559}{10.75} \times 100\% = 5.2\%$$

and the average power at the fundamental frequency is

$$0.5 \times \frac{10.75^2}{100} = 0.5778 \text{ W}$$

SOLUTION TO PROBLEM 22.19.

$$v_o(t) = V_0 + V_1 \cos(\omega t) + V_2 \cos(2\omega t) + V_3 \cos(3\omega t)$$

We use equation 22.30 and the values of $v_o(t)$ read from the oscilloscope to compute V_k . The total harmonic distortion is given by

$$\text{H.D.} = \frac{\sqrt{V_2^2 + V_3^2}}{|V_1|} \times 100 \%$$

MATLAB codes:

```
vo0= 10; vo60= 5.2; vo120= -4.6; vo180= -9.6;
V0= (vo0+2*vo60+2*vo120 +vo180)/6
V1= (vo0+ vo60 - vo120 -vo180)/3
V2= (vo0 - vo60 - vo120 +vo180)/3
V3= (vo0-2*vo60+2*vo120 -vo180)/6
% total harmonic distortion
HD= 100*sqrt( V2^2 +V3^2)/V1
```

The following answers are obtained from MATLAB output.

```
V0 = 0.2667 V
V1 = 9.8000 V
V2 = -0.0667
V3 = 0 V
HD = 0.6803 (percent)
```

SOLUTION PROBLEM 22.20.

We shall follow the solution given in example 22.12, and only indicate the needed changes below. There are two corrections in example 22.12: (1) $20\cos(\omega t)$ should be $20\cos(0.5\omega t)$ and (2) $1.842\cos(\omega t)$ should be $1.842\cos(3\omega t)$.

The new input is

$$v_i(t) = 0.9 \cos(6000t)$$

The positive peak of the output sine wave is clipped for $\omega t = T$.

$$0.9 \times 20 \cos(0.5 \pi T) = 15 = \cos^{-1}(15/18) = 0.1864$$

Equation 22.35 becomes

$$v_0(t) = -1.8 \cos(\omega t) + 2\alpha_1 \cos(\omega t) + 2\alpha_3 \cos(3\omega t) + 2\alpha_5 \cos(5\omega t) + \dots$$

Equation 2.36 becomes

$$v_{pp}(t) = [1.8 \cos(\omega t) - 15] f_p(t)$$

Using $A=1$, and $\theta = 0.1864$ item #2 of table 22.4, equation 22.37 becomes

$$f_p(t) = 0.1864 + 0.316 \cos(\omega t) + 0.293 \cos(2\omega t) + 0.208 \cos(3\omega t) \\ + 0.114 \cos(4\omega t) + 0.0269 \cos(5\omega t) - 0.0386 \cos(6\omega t) + \dots$$

and equation 22.38 becomes

$$v_{pp}(t) = 0.7164 \cos(\omega t) + 0.5376 \cos(3\omega t) + 0.2748 \cos(5\omega t) + \\ \text{higher order odd harmonics} + \text{even harmonics}$$

Equation 22.39 becomes

$$v_0(t) = -16.57 \cos(\omega t) + 1.076 \cos(3\omega t) + 0.55 \cos(5\omega t) \\ + \text{higher order odd harmonics.}$$

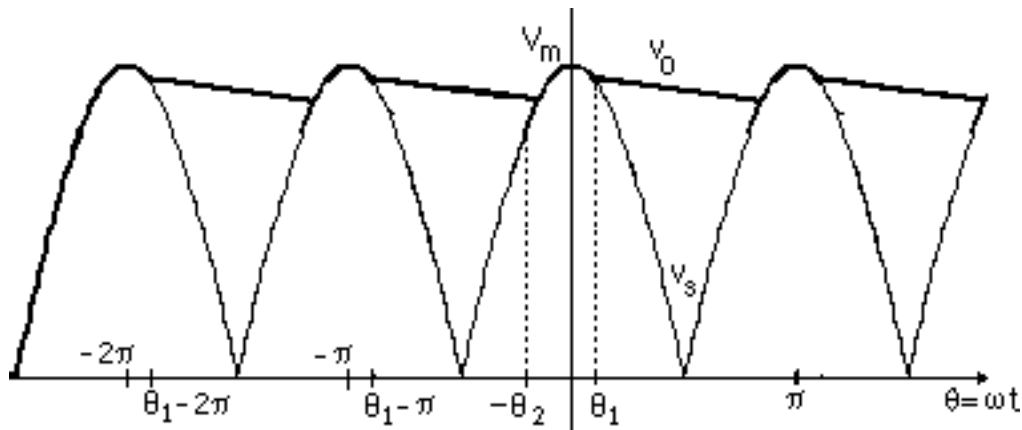
from which the harmonic distortions are:

third order	$1.076/16.57 = 6.595\%$
fifth order	$0.55/16.57 = 3.319\%$

SOLUTION PROBLEM 22.21. Corrections: (1) $\cos(\theta_1)e^{-\frac{-\theta_2 - \theta_1 +}{\omega RC}} = \cos(\theta_2)$ should be $\cos(\theta_1)e^{-\frac{-\theta_2 - \theta_1 +}{\omega RC}} = \cos(\theta_2)$ and (2) on page 943, equation 22.46, θ_2 should be $-\theta_2$, i.e., equation 22.46 should be $\cos(\theta_1)e^{-\frac{-\theta_2 - \theta_1 +}{\omega RC}}$.

The proof is similar to that given on page 943 for the half-wave rectifier case, except for some minor changes described below.

For the case of a full-wave rectifier, the output voltage waveform is a modification of figure 22.17 as shown below.



The exponential decay of $v_o(t)$ starts with the value $V_m \cos(\theta_1)$ at $\theta = \theta_1 - \pi$ (instead of $\theta_1 - 2\pi$, as in the half-wave rectifier case). Therefore, in equation 22.45, change T to $T/2$ and θ_2 to $-\theta_2$. In other words

$$v_o(t) = \left(V_m \cos(\theta_1) \right) e^{-\frac{t - \frac{\theta_1}{\omega} - \frac{T}{2}}{RC}} = \left(V_m \cos(\theta_1) \right) e^{-\frac{\omega t - (\theta_1 - \pi)}{\omega RC}}$$

In equation 22.46, make correction (2) above, and change θ_2 to $-\theta_2$, i.e.,

$$\cos(\theta_1) e^{-\frac{-\theta_2 - \theta_1 +}{\omega RC}} = \cos(\theta_2)$$

The desired proof is complete.

SOLUTION PROBLEM P22.22

Refer to figure 22.17. Assuming $\phi_1 = 0$, we have

$$v_0(t) = V_m \exp\left(-\frac{t}{RC}\right) = V_m \left\{ 1 - \left(\frac{t}{RC}\right) + \left(\frac{t}{RC}\right)^2 - \left(\frac{t}{RC}\right)^3 + \dots \right\}$$

Assuming $\phi_2 = 0$, we compute the average value of $v_0(t)$ over the time interval $[0, T]$. For the case $RC \gg T$, we can approximate $v_0(t)$ over this interval by keeping only the first two terms of the infinite series. Thus

$$v_0(t) \approx V_m \left[1 - \frac{t}{RC} \right]$$

which indicates that the plot of v_0 vs. t over the interval $[0, T]$ is approximately a straight line. Therefore the average of the $v_0(t)$ over $[0, T]$ is equal to $v_0(T/2)$. Thus, for the case $RC \gg T$, or equivalently $RC \gg 2\pi$,

$$V_{dc} = v_0\left(\frac{T}{2}\right) = V_m \left[1 - \frac{T}{2RC} \right] = V_m \left[1 - \frac{1}{2fRC} \right]$$

SOLUTION PROBLEM 22.23

Given values are: $C = 20 \times 10^{-6} \text{ F}$, $R = 100 \text{ k}\Omega$, $V_m = 20 \text{ V}$; $f = 60 \text{ Hz}$. From equation 22.48b

$$V_{dc} = \left(1 - \frac{1}{2fRC}\right) V_m = \left(1 - \frac{1}{2 \times 60 \times 10^5 \times 20 \times 10^{-6}}\right) \times 20 = 19.916 \text{ V}$$

To calculate the ripple factor, we first calculate ϕ_2 from equation 22.47, and then use the result in equation 22.50.

$$\phi_2 = \cos^{-1}\left(\frac{2}{RC}\right) = 0.1289 \text{ rad}$$

$$\text{ripple factor} = \frac{1 - \cos(\alpha)}{\sqrt{3} [1 + \cos(\alpha)]} = 0.2406\%$$

For the diode average and peak currents, use equations 22.49a and 22.52

$$I_{dc} = \frac{V_{dc}}{R} = \frac{19.917}{100,000} = 0.199 \times 10^{-3} \text{ A}$$

$$i_{d,peak} = V_m \sin(\alpha) = 19.4 \times 10^{-3} \text{ A}$$

SOLUTION PROBLEM 22.24

Equations 22.44 - 22.52 are derived for a half-wave rectifier. For a full-wave rectifier, some of these equations be modified slightly as given below. The difference arises from changing T to T/2.

The new equation for α is derived in problem 22.21, and repeated below.

The given values are: $C = 20 \times 10^{-6} \text{ F}$, $R = 100 \text{ k}$, $V_m = 20 \text{ V}$; $f = 60 \text{ Hz}$.

A modification of equation 22.48b gives

$$V_{dc} = \left(1 - \frac{T}{2RC}\right)V_m = \left(1 - \frac{T}{4RC}\right)V_m = \left(1 - \frac{1}{4 \times 60 \times 10^5 \times 20 \times 10^{-6}}\right) \times 20 = 19.96 \text{ V}$$

To calculate the ripple factor, we first calculate α from equation derived in problem 22.21, and then use the result in equation 22.50.

$$\alpha = \cos^{-1}\left(e^{-\frac{T}{RC}}\right) = 5.23 \text{ degrees}$$

$$\text{ripple factor} = \frac{1 - \cos(\alpha)}{\sqrt{3} [1 + \cos(\alpha)]} = 0.12\%$$

For the diode average and peak currents, use equations 22.49a and 22.52

$$I_{dc} = \frac{V_{dc}}{R} = \frac{19.96}{100,000} = 0.1996 \times 10^{-3} \text{ A}$$

$$i_{d,peak} = V_m \sin(\alpha) = 13.75 \times 10^{-3} \text{ A}$$

SOLUTION PROBLEM 22.25. CORRECTIONS: (1) 195 should be 1950 . (2) 100 μF should be 10 μF .

Since this problem only requires an estimate of the answer, we can use reasonable approximations to simplify the solution. Let $H(s) = V_o(s)/I(s)$ be the transfer function for the linear circuit to the right of the diodes. The

$$H(s) = \frac{V_{in}(s)}{I(s)} \times \frac{V_o(s)}{V_{in}(s)} = Z_{in}(s) \frac{Z_{par}(s)}{R + Z_{par}(s)}$$

where $Z_{par}(s)$ is the impedance of the parallel C- R_L .

The first step is to find the magnitude $|H(j\omega)|$. As long as $1/R_L \ll \omega C$ and $1/(\omega C) \ll R$, the following approximations are valid:

$$|Z_{par}(j\omega)| = \left| \frac{1}{j\omega C + \frac{1}{R_L}} \right| \approx \frac{1}{\omega C}$$

which means that the parallel impedance is essentially that of the capacitor, and

$$\left| \frac{Z_{par}(j\omega)}{R + Z_{par}(j\omega)} \right| \approx \left| \frac{Z_{par}(j\omega)}{R} \right| \approx \frac{1}{\omega RC}$$

and again since $1/(\omega C) \ll R$,

$$|Z_{in}(j\omega)| \approx \frac{1}{\omega C}$$

Using these approximations,

$$|H(j\omega)| = |Z_{in}(j\omega)| \times \left| \frac{Z_{par}(j\omega)}{R + Z_{par}(j\omega)} \right| \approx \frac{1}{\omega C} \times \frac{1}{\omega RC} = \frac{R}{(\omega RC)^2}$$

It is given that $I_{dc} = 0.01$ A. From the short pulse property, the input current $i(t)$ consists of very short pulses at 120 Hz and all ac components of $i(t)$ have peak magnitudes approximately equal to twice the average dc value. Hence the peak magnitudes are 0.02 A. Therefore the magnitude of 120-Hz component of the output voltage

$$|H(j2\pi \times 120)| \times 0.02 = \frac{R}{(\omega RC)^2} \times 0.02 = \frac{1950}{(2\pi \times 120 \times 1950 \times 10 \times 10^{-6})^2} \times 0.02 = 0.18042 \text{ V}$$

Hence, the effective value is $0.18042/\sqrt{2} = 0.12757$ V and the ripple factor is

$$\frac{0.12757}{30} \times 100 = 0.42524 \%$$

SOLUTION PROBLEM 22.26

Since this problem only requires an estimate of the answer, we can use reasonable approximations to simplify the solution. Let $H(s) = V_o(s)/I(s)$ be the transfer function for the linear circuit to the right of the diodes. Then

$$H(s) = \frac{V_o}{I} = \frac{V_{in}}{I} \times \frac{V_o}{V_{in}}$$

Under the condition $1/(C) \ll R$ and $1/(C) \ll R_L$, we have

$$Z_{in}(s) \approx Z_C(s) = \frac{1}{Cs}$$

and
$$\frac{V_o}{V_{in}} \approx \left(-\frac{1}{RC}\right)^2$$

Using these approximations,

$$|H(j\omega)| \approx |Z_{in}| \left| \frac{V_{out}}{V_{in}} \right| = \frac{1}{C} \left(-\frac{1}{RC}\right)^2 = R \left(-\frac{1}{RC}\right)^3$$

For a full-wave rectifier, the fundamental frequency is 120 Hz, and $\omega = 240$ rad/s. It is given that $I_{dc} = 0.01$ A. From the short pulse property, the input current $i(t)$ consists of very short pulses at 120 Hz and all ac components of $i(t)$ have peak magnitudes approximately equal to twice the average dc value. Hence the peak magnitudes are 0.02 A. Therefore the peak magnitude of 120-Hz component of the output voltage is

$$|H(j120)| \times 0.02 = R \left(-\frac{1}{RC}\right)^3 \times 0.02 = 975 \times \left(\frac{1}{120 \times 975 \times 16 \times 10^{-6}}\right)^3 \times 0.02 = 0.012 \text{ V}$$

Hence, the effective value is $0.012/\sqrt{2} = 0.00848$ V and the ripple factor is

$$\frac{0.0848}{30} \times 100\% = 0.2827\%$$

SOLUTION PROBLEM 22.27

Using $H(j\omega)$ of figure P22.27 and the given formula for c_n , we have

$$c_n = \frac{1}{s} \int_{-0.5s}^{0.5s} H(j\omega) e^{-jnT_0} d\omega = \frac{1}{s} \int_{-0.25s}^{0.25s} e^{-jnT_0} d\omega = \frac{1}{-jnT_0 s} [e^{-jnT_0 \omega}]_{-0.25s}^{0.25s}$$

$$= \frac{1}{n} \sin\left(\frac{n\pi}{2}\right), \quad n = 1, 2, \dots$$

For $n = 0$, we have $c_0 = d_0 = a_0/2 = [\text{Average value of } H(j\omega)] = 0.5$.

For $n = 1, 2, \dots$, from equation 22.6

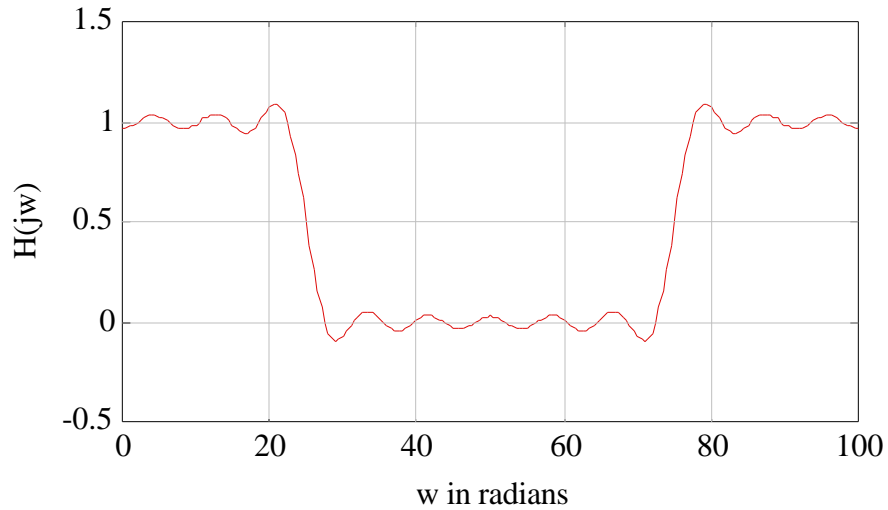
$$b_n = 0,$$

$$d_n = a_n = \frac{2}{n} \sin\left(\frac{n\pi}{2}\right),$$

The Fourier series representation of $H(j\omega)$ is

$$H(j\omega) = 0.5 + 2 \left[\cos(T_0 \omega) - \frac{1}{3} \cos(3T_0 \omega) + \frac{1}{5} \cos(5T_0 \omega) - \frac{1}{7} \cos(7T_0 \omega) + \dots \right]$$

A plot of $H(j\omega)$ vs. ω curve using the first 11 terms ($n=0, 1, \dots, 11$) of the Fourier series is given below together with the MATLAB codes.



```

%chapter 2, problem 27.
ws= 100;
T0=2*pi/ws;
w= 0: ws/200:ws;
d0w = 0.5;
d1w = (2/pi)*cos(T0*w);
d3w= -(2/pi/3)*cos(3*T0*w);
d5w= (2/pi/5)*cos(5*T0*w);
d7w= -(2/pi/7)*cos(7*T0*w);
d9w= +(2/pi/9)*cos(9*T0*w);
d11w= -(2/pi/10)*cos(11*T0*w);
H =d0w +d1w + d3w +d5w +d7w + d9w +d11w;
plot(w,H)
xlabel(' w in radians')
ylabel('H(jw)')
grid

```